

1. (a) The charge that passes through any cross section is the product of the current and time. Since  $4.0 \text{ min} = (4.0 \text{ min})(60 \text{ s/min}) = 240 \text{ s}$ ,  $q = it = (5.0 \text{ A})(240 \text{ s}) = 1.2 \times 10^3 \text{ C}$ .

(b) The number of electrons  $N$  is given by  $q = Ne$ , where  $e$  is the magnitude of the charge on an electron. Thus,

$$N = q/e = (1200 \text{ C})/(1.60 \times 10^{-19} \text{ C}) = 7.5 \times 10^{21}.$$

2. We adapt the discussion in the text to a moving two-dimensional collection of charges. Using  $\sigma$  for the charge per unit area and  $w$  for the belt width, we can see that the transport of charge is expressed in the relationship  $i = \sigma vw$ , which leads to

$$\sigma = \frac{i}{vw} = \frac{100 \times 10^{-6} \text{ A}}{(30 \text{ m/s})(50 \times 10^{-2} \text{ m})} = 6.7 \times 10^{-6} \text{ C/m}^2.$$

3. Suppose the charge on the sphere increases by  $\Delta q$  in time  $\Delta t$ . Then, in that time its potential increases by

$$\Delta V = \frac{\Delta q}{4\pi\epsilon_0 r},$$

where  $r$  is the radius of the sphere. This means

$$\Delta q = 4\pi\epsilon_0 r \Delta V.$$

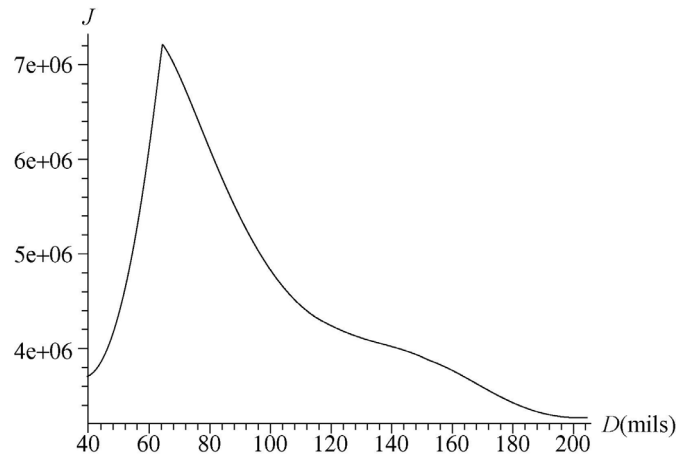
Now,  $\Delta q = (i_{\text{in}} - i_{\text{out}}) \Delta t$ , where  $i_{\text{in}}$  is the current entering the sphere and  $i_{\text{out}}$  is the current leaving. Thus,

$$\begin{aligned}\Delta t &= \frac{\Delta q}{i_{\text{in}} - i_{\text{out}}} = \frac{4\pi\epsilon_0 r \Delta V}{i_{\text{in}} - i_{\text{out}}} \\ &= \frac{(0.10 \text{ m})(1000 \text{ V})}{(8.99 \times 10^9 \text{ F/m})(1.0000020 \text{ A} - 1.0000000 \text{ A})} = 5.6 \times 10^{-3} \text{ s}.\end{aligned}$$

4. We express the magnitude of the current density vector in SI units by converting the diameter values in mils to inches (by dividing by 1000) and then converting to meters (by multiplying by 0.0254) and finally using

$$J = \frac{i}{A} = \frac{i}{\pi R^2} = \frac{4i}{\pi D^2}.$$

For example, the gauge 14 wire with  $D = 64 \text{ mil} = 0.0016 \text{ m}$  is found to have a (maximum safe) current density of  $J = 7.2 \times 10^6 \text{ A/m}^2$ . In fact, this is the wire with the largest value of  $J$  allowed by the given data. The values of  $J$  in SI units are plotted below as a function of their diameters in mils.



5. (a) The magnitude of the current density is given by  $J = nqv_d$ , where  $n$  is the number of particles per unit volume,  $q$  is the charge on each particle, and  $v_d$  is the drift speed of the particles. The particle concentration is  $n = 2.0 \times 10^8/\text{cm}^3 = 2.0 \times 10^{14} \text{ m}^{-3}$ , the charge is

$$q = 2e = 2(1.60 \times 10^{-19} \text{ C}) = 3.20 \times 10^{-19} \text{ C},$$

and the drift speed is  $1.0 \times 10^5 \text{ m/s}$ . Thus,

$$J = (2 \times 10^{14} / \text{m}^3)(3.2 \times 10^{-19} \text{ C})(1.0 \times 10^5 \text{ m/s}) = 6.4 \text{ A/m}^2.$$

(b) Since the particles are positively charged the current density is in the same direction as their motion, to the north.

(c) The current cannot be calculated unless the cross-sectional area of the beam is known. Then  $i = JA$  can be used.

6. (a) The magnitude of the current density vector is

$$J = \frac{i}{A} = \frac{i}{\pi d^2 / 4} = \frac{4(1.2 \times 10^{-10} \text{ A})}{\pi(2.5 \times 10^{-3} \text{ m})^2} = 2.4 \times 10^{-5} \text{ A / m}^2.$$

(b) The drift speed of the current-carrying electrons is

$$v_d = \frac{J}{ne} = \frac{2.4 \times 10^{-5} \text{ A / m}^2}{(8.47 \times 10^{28} / \text{m}^3)(1.60 \times 10^{-19} \text{ C})} = 1.8 \times 10^{-15} \text{ m / s}.$$

7. The cross-sectional area of wire is given by  $A = \pi r^2$ , where  $r$  is its radius (half its thickness). The magnitude of the current density vector is  $J = i / A = i / \pi r^2$ , so

$$r = \sqrt{\frac{i}{\pi J}} = \sqrt{\frac{0.50 \text{ A}}{\pi(440 \times 10^4 \text{ A / m}^2)}} = 1.9 \times 10^{-4} \text{ m}.$$

The diameter of the wire is therefore  $d = 2r = 2(1.9 \times 10^{-4} \text{ m}) = 3.8 \times 10^{-4} \text{ m}$ .

8. (a) Since  $1 \text{ cm}^3 = 10^{-6} \text{ m}^3$ , the magnitude of the current density vector is

$$J = nev = \left( \frac{8.70}{10^{-6} \text{ m}^3} \right) (1.60 \times 10^{-19} \text{ C}) (470 \times 10^3 \text{ m/s}) = 6.54 \times 10^{-7} \text{ A/m}^2.$$

(b) Although the total surface area of Earth is  $4\pi R_E^2$  (that of a sphere), the area to be used in a computation of how many protons in an approximately unidirectional beam (the solar wind) will be captured by Earth is its projected area. In other words, for the beam, the encounter is with a “target” of circular area  $\pi R_E^2$ . The rate of charge transport implied by the influx of protons is

$$i = AJ = \pi R_E^2 J = \pi (6.37 \times 10^6 \text{ m})^2 (6.54 \times 10^{-7} \text{ A/m}^2) = 8.34 \times 10^7 \text{ A}.$$



9. We use  $v_d = J/ne = i/Ane$ . Thus,

$$\begin{aligned} t &= \frac{L}{v_d} = \frac{L}{i/Ane} = \frac{LANe}{i} = \frac{(0.85\text{ m}) (0.21 \times 10^{-14} \text{ m}^2) (8.47 \times 10^{28} / \text{m}^3) (1.60 \times 10^{-19} \text{ C})}{300 \text{ A}} \\ &= 8.1 \times 10^2 \text{ s} = 13 \text{ min.} \end{aligned}$$

10. We note that the radial width  $\Delta r = 10 \text{ }\mu\text{m}$  is small enough (compared to  $r = 1.20 \text{ mm}$ ) that we can make the approximation

$$\int Br \, 2\pi r \, dr \approx Br \, 2\pi r \, \Delta r .$$

Thus, the enclosed current is  $2\pi Br^2 \Delta r = 18.1 \text{ }\mu\text{A}$ . Performing the integral gives the same answer.

11. (a) The current resulting from this non-uniform current density is

$$i = \int_{\text{cylinder}} J_a dA = \frac{J_0}{R} \int_0^R r \cdot 2\pi r dr = \frac{2}{3} \pi R^2 J_0 = \frac{2}{3} \pi (3.40 \times 10^{-3} \text{ m})^2 (5.50 \times 10^4 \text{ A/m}^2) = 1.33 \text{ A}.$$

(b) In this case,

$$i = \int_{\text{cylinder}} J_b dA = \int_0^R J_0 \left(1 - \frac{r}{R}\right) 2\pi r dr = \frac{1}{3} \pi R^2 J_0 = \frac{1}{3} \pi (3.40 \times 10^{-3} \text{ m})^2 (5.50 \times 10^4 \text{ A/m}^2) \\ = 0.666 \text{ A}.$$

(c) The result is different from that in part (a) because  $J_b$  is higher near the center of the cylinder (where the area is smaller for the same radial interval) and lower outward, resulting in a lower average current density over the cross section and consequently a lower current than that in part (a). So,  $J_a$  has its maximum value near the surface of the wire.

12. Assuming  $\vec{J}$  is directed along the wire (with no radial flow) we integrate, starting with Eq. 26-4,

$$i = \int |\vec{J}| dA = \int_{R/10}^R (kr^2) 2\pi r dr = \frac{1}{2} k\pi (R^4 - 0.656R^4)$$

where  $k = 3.0 \times 10^8$  and SI units understood. Therefore, if  $R = 0.00200$  m, we obtain  $i = 2.59 \times 10^{-3}$  A .

13. We find the conductivity of Nichrome (the reciprocal of its resistivity) as follows:

$$\sigma = \frac{1}{\rho} = \frac{L}{RA} = \frac{L}{(V/i)A} = \frac{Li}{VA} = \frac{(1.0 \text{ m})(4.0 \text{ A})}{(2.0 \text{ V})(1.0 \times 10^{-6} \text{ m}^2)} = 2.0 \times 10^6 / \Omega \cdot \text{m}.$$

14. We use  $R/L = \rho/A = 0.150 \text{ } \Omega/\text{km}$ .

(a) For copper  $J = i/A = (60.0 \text{ A})(0.150 \text{ } \Omega/\text{km})/(1.69 \times 10^{-8} \text{ } \Omega \cdot \text{m}) = 5.32 \times 10^5 \text{ A/m}^2$ .

(b) We denote the mass densities as  $\rho_m$ . For copper,

$$(m/L)_c = (\rho_m A)_c = (8960 \text{ kg/m}^3) (1.69 \times 10^{-8} \text{ } \Omega \cdot \text{m})/(0.150 \text{ } \Omega/\text{km}) = 1.01 \text{ kg/m}.$$

(c) For aluminum  $J = (60.0 \text{ A})(0.150 \text{ } \Omega/\text{km})/(2.75 \times 10^{-8} \text{ } \Omega \cdot \text{m}) = 3.27 \times 10^5 \text{ A/m}^2$ .

(d) The mass density of aluminum is

$$(m/L)_a = (\rho_m A)_a = (2700 \text{ kg/m}^3)(2.75 \times 10^{-8} \text{ } \Omega \cdot \text{m})/(0.150 \text{ } \Omega/\text{km}) = 0.495 \text{ kg/m}.$$

15. The resistance of the wire is given by  $R = \rho L / A$ , where  $\rho$  is the resistivity of the material,  $L$  is the length of the wire, and  $A$  is its cross-sectional area. In this case,

$$A = \pi r^2 = \pi (0.50 \times 10^{-3} \text{ m})^2 = 7.85 \times 10^{-7} \text{ m}^2.$$

Thus,

$$\rho = \frac{RA}{L} = \frac{(50 \times 10^{-3} \Omega) (7.85 \times 10^{-7} \text{ m}^2)}{2.0 \text{ m}} = 2.0 \times 10^{-8} \Omega \cdot \text{m}.$$

16. (a)  $i = V/R = 23.0 \text{ V}/15.0 \times 10^{-3} \Omega = 1.53 \times 10^3 \text{ A}$ .

(b) The cross-sectional area is  $A = \pi r^2 = \frac{1}{4} \pi D^2$ . Thus, the magnitude of the current density vector is

$$J = \frac{i}{A} = \frac{4i}{\pi D^2} = \frac{4(1.53 \times 10^3 \text{ A})}{\pi(6.00 \times 10^{-3} \text{ m})^2} = 5.41 \times 10^7 \text{ A/m}^2.$$

(c) The resistivity is

$$\rho = RA/L = (15.0 \times 10^{-3} \Omega)(\pi)(6.00 \times 10^{-3} \text{ m})^2 / [4(4.00 \text{ m})] = 10.6 \times 10^{-8} \Omega \cdot \text{m}.$$

(d) The material is platinum.



17. Since the potential difference  $V$  and current  $i$  are related by  $V = iR$ , where  $R$  is the resistance of the electrician, the fatal voltage is  $V = (50 \times 10^{-3} \text{ A})(2000 \, \Omega) = 100 \text{ V}$ .

18. The thickness (diameter) of the wire is denoted by  $D$ . We use  $R \propto L/A$  (Eq. 26-16) and note that  $A = \frac{1}{4}\pi D^2 \propto D^2$ . The resistance of the second wire is given by

$$R_2 = R \left( \frac{A_1}{A_2} \right) \left( \frac{L_2}{L_1} \right) = R \left( \frac{D_1}{D_2} \right)^2 \left( \frac{L_2}{L_1} \right) = R(2)^2 \left( \frac{1}{2} \right) = 2R.$$

19. The resistance of the coil is given by  $R = \rho L/A$ , where  $L$  is the length of the wire,  $\rho$  is the resistivity of copper, and  $A$  is the cross-sectional area of the wire. Since each turn of wire has length  $2\pi r$ , where  $r$  is the radius of the coil, then

$$L = (250)2\pi r = (250)(2\pi)(0.12 \text{ m}) = 188.5 \text{ m}.$$

If  $r_w$  is the radius of the wire itself, then its cross-sectional area is  $A = \pi r_w^2 = \pi(0.65 \times 10^{-3} \text{ m})^2 = 1.33 \times 10^{-6} \text{ m}^2$ . According to Table 26-1, the resistivity of copper is  $1.69 \times 10^{-8} \Omega \cdot \text{m}$ . Thus,

$$R = \frac{\rho L}{A} = \frac{(1.69 \times 10^{-8} \Omega \cdot \text{m})(188.5 \text{ m})}{1.33 \times 10^{-6} \text{ m}^2} = 2.4 \Omega.$$

20. (a) Since the material is the same, the resistivity  $\rho$  is the same, which implies (by Eq. 26-11) that the electric fields (in the various rods) are directly proportional to their current-densities. Thus,  $J_1: J_2: J_3$  are in the ratio 2.5/4/1.5 (see Fig. 26-24). Now the currents in the rods must be the same (they are “in series”) so

$$J_1 A_1 = J_3 A_3 \quad \text{and} \quad J_2 A_2 = J_3 A_3 \quad .$$

Since  $A = \pi r^2$  this leads (in view of the aforementioned ratios) to

$$4r_2^2 = 1.5r_3^2 \quad \text{and} \quad 2.5r_1^2 = 1.5r_3^2 \quad .$$

Thus, with  $r_3 = 2$  mm, the latter relation leads to  $r_1 = 1.55$  mm.

(b) The  $4r_2^2 = 1.5r_3^2$  relation leads to  $r_2 = 1.22$  mm.

21. Since the mass density of the material do not change, the volume remains the same. If  $L_0$  is the original length,  $L$  is the new length,  $A_0$  is the original cross-sectional area, and  $A$  is the new cross-sectional area, then  $L_0 A_0 = LA$  and  $A = L_0 A_0 / L = L_0 A_0 / 3L_0 = A_0 / 3$ . The new resistance is

$$R = \frac{\rho L}{A} = \frac{\rho 3L_0}{A_0 / 3} = 9 \frac{\rho L_0}{A_0} = 9R_0,$$

where  $R_0$  is the original resistance. Thus,  $R = 9(6.0 \, \Omega) = 54 \, \Omega$ .

22. The cross-sectional area is  $A = \pi r^2 = \pi(0.002 \text{ m})^2$ . The resistivity from Table 26-1 is  $\rho = 1.69 \times 10^{-8} \Omega \cdot \text{m}$ . Thus, with  $L = 3 \text{ m}$ , Ohm's Law leads to  $V = iR = i\rho L/A$ , or

$$12 \times 10^{-6} \text{ V} = i(1.69 \times 10^{-8} \Omega \cdot \text{m})(3.0 \text{ m}) / \pi(0.002 \text{ m})^2$$

which yields  $i = 0.00297 \text{ A}$  or roughly  $3.0 \text{ mA}$ .

23. The resistance of conductor  $A$  is given by

$$R_A = \frac{\rho L}{\pi r_A^2},$$

where  $r_A$  is the radius of the conductor. If  $r_o$  is the outside diameter of conductor  $B$  and  $r_i$  is its inside diameter, then its cross-sectional area is  $\pi(r_o^2 - r_i^2)$ , and its resistance is

$$R_B = \frac{\rho L}{\pi(r_o^2 - r_i^2)}.$$

The ratio is

$$\frac{R_A}{R_B} = \frac{r_o^2 - r_i^2}{r_A^2} = \frac{(1.0 \text{ mm})^2 - (0.50 \text{ mm})^2}{(0.50 \text{ mm})^2} = 3.0.$$

24. The absolute values of the slopes (for the straight-line segments shown in the graph of Fig. 26-26(b)) are equal to the respective electric field magnitudes. Thus, applying Eq. 26-5 and Eq. 26-13 to the three sections of the resistive strip, we have

$$J_1 = \frac{i}{A} = \sigma_1 E_1 = \sigma_1 (0.50 \times 10^3 \text{ V/m})$$

$$J_2 = \frac{i}{A} = \sigma_2 E_2 = \sigma_2 (4.0 \times 10^3 \text{ V/m})$$

$$J_3 = \frac{i}{A} = \sigma_3 E_3 = \sigma_3 (1.0 \times 10^3 \text{ V/m}) .$$

We note that the current densities are the same since the values of  $i$  and  $A$  are the same (see the problem statement) in the three sections, so  $J_1 = J_2 = J_3$ .

(a) Thus we see that

$$\sigma_1 = 2\sigma_3 = 2 (3.00 \times 10^7 (\Omega \cdot \text{m})^{-1}) = 6.00 \times 10^7 (\Omega \cdot \text{m})^{-1} .$$

(b) Similarly,  $\sigma_2 = \sigma_3/4 = (3.00 \times 10^7 (\Omega \cdot \text{m})^{-1})/4 = 7.50 \times 10^6 (\Omega \cdot \text{m})^{-1}$ .



25. The resistance at operating temperature  $T$  is  $R = V/i = 2.9 \text{ V}/0.30 \text{ A} = 9.67 \text{ } \Omega$ . Thus, from  $R - R_0 = R_0 \alpha (T - T_0)$ , we find

$$T = T_0 + \frac{1}{\alpha} \left( \frac{R}{R_0} - 1 \right) = 20^\circ\text{C} + \left( \frac{1}{4.5 \times 10^{-3} / \text{K}} \right) \left( \frac{9.67 \text{ } \Omega}{1.1 \text{ } \Omega} - 1 \right) = 1.9 \times 10^3 \text{ } ^\circ\text{C}.$$

Since a change in Celsius is equivalent to a change on the Kelvin temperature scale, the value of  $\alpha$  used in this calculation is not inconsistent with the other units involved. Table 26-1 has been used.

26. First we find  $R = \rho L/A = 2.69 \times 10^{-5} \Omega$ . Then  $i = V/R = 1.115 \times 10^{-4} \text{ A}$ . Finally,  $\Delta Q = i \Delta t = 3.35 \times 10^{-7} \text{ C}$ .

27. We use  $J = E/\rho$ , where  $E$  is the magnitude of the (uniform) electric field in the wire,  $J$  is the magnitude of the current density, and  $\rho$  is the resistivity of the material. The electric field is given by  $E = V/L$ , where  $V$  is the potential difference along the wire and  $L$  is the length of the wire. Thus  $J = V/L\rho$  and

$$\rho = \frac{V}{LJ} = \frac{115 \text{ V}}{(10 \text{ m})(1.4 \times 10^4 \text{ A/m}^2)} = 8.2 \times 10^{-4} \Omega \cdot \text{m}.$$

28. We use  $J = \sigma E = (n_+ + n_-)ev_d$ , which combines Eq. 26-13 and Eq. 26-7.

(a)  $J = \sigma E = (2.70 \times 10^{-14} / \Omega \cdot \text{m}) (120 \text{ V/m}) = 3.24 \times 10^{-12} \text{ A/m}^2$ .

(b) The drift velocity is

$$v_d = \frac{\sigma E}{(n_+ + n_-)e} = \frac{(2.70 \times 10^{-14} / \Omega \cdot \text{m})(120 \text{ V/m})}{[(620 + 550) / \text{cm}^3](1.60 \times 10^{-19} \text{ C})} = 1.73 \text{ cm/s}.$$

29. (a)  $i = V/R = 35.8 \text{ V}/935 \, \Omega = 3.83 \times 10^{-2} \text{ A}$ .

(b)  $J = i/A = (3.83 \times 10^{-2} \text{ A})/(3.50 \times 10^{-4} \text{ m}^2) = 109 \text{ A/m}^2$ .

(c)  $v_d = J/ne = (109 \text{ A/m}^2)/[(5.33 \times 10^{22}/\text{m}^3) (1.60 \times 10^{-19} \text{ C})] = 1.28 \times 10^{-2} \text{ m/s}$ .

(d)  $E = V/L = 35.8 \text{ V}/0.158 \text{ m} = 227 \text{ V/m}$ .

30. We use  $R \propto L/A$ . The diameter of a 22-gauge wire is  $1/4$  that of a 10-gauge wire. Thus from  $R = \rho L/A$  we find the resistance of 25 ft of 22-gauge copper wire to be

$$R = (1.00 \, \Omega) (25 \, \text{ft}/1000 \, \text{ft})(4)^2 = 0.40 \, \Omega.$$

31. (a) The current in each strand is  $i = 0.750 \text{ A}/125 = 6.00 \times 10^{-3} \text{ A}$ .

(b) The potential difference is  $V = iR = (6.00 \times 10^{-3} \text{ A}) (2.65 \times 10^{-6} \Omega) = 1.59 \times 10^{-8} \text{ V}$ .

(c) The resistance is  $R_{\text{total}} = 2.65 \times 10^{-6} \Omega/125 = 2.12 \times 10^{-8} \Omega$ .

32. The number density of conduction electrons in copper is  $n = 8.49 \times 10^{28} / \text{m}^3$ . The electric field in section 2 is  $(10.0 \text{ } \mu\text{V}) / (2.00 \text{ m}) = 5.00 \text{ } \mu\text{V/m}$ . Since  $\rho = 1.69 \times 10^{-8} \text{ } \Omega \cdot \text{m}$  for copper (see Table 26-1) then Eq. 26-10 leads to a current density vector of magnitude  $J_2 = (5.00 \text{ } \mu\text{V/m}) / (1.69 \times 10^{-8} \text{ } \Omega \cdot \text{m}) = 296 \text{ A/m}^2$  in section 2. Conservation of electric current from section 1 into section 2 implies

$$J_1 A_1 = J_2 A_2$$

$$J_1 (4\pi R^2) = J_2 (\pi R^2)$$

(see Eq. 26-5). This leads to  $J_1 = 74 \text{ A/m}^2$ . Now, Eq. 26-7 immediately yields

$$v_d = \frac{J_1}{ne} = 5.44 \times 10^{-9} \text{ m/s}$$

for the drift speed of conduction-electrons in section 1.



33. (a) The current  $i$  is shown in Fig. 26-29 entering the truncated cone at the left end and leaving at the right. This is our choice of positive  $x$  direction. We make the assumption that the current density  $J$  at each value of  $x$  may be found by taking the ratio  $i/A$  where  $A = \pi r^2$  is the cone's cross-section area at that particular value of  $x$ . The direction of  $\vec{J}$  is identical to that shown in the figure for  $i$  (our  $+x$  direction). Using Eq. 26-11, we then find an expression for the electric field at each value of  $x$ , and next find the potential difference  $V$  by integrating the field along the  $x$  axis, in accordance with the ideas of Chapter 25. Finally, the resistance of the cone is given by  $R = V/i$ . Thus,

$$J = \frac{i}{\pi r^2} = \frac{E}{\rho}$$

where we must deduce how  $r$  depends on  $x$  in order to proceed. We note that the radius increases linearly with  $x$ , so (with  $c_1$  and  $c_2$  to be determined later) we may write

$$r = c_1 + c_2 x.$$

Choosing the origin at the left end of the truncated cone, the coefficient  $c_1$  is chosen so that  $r = a$  (when  $x = 0$ ); therefore,  $c_1 = a$ . Also, the coefficient  $c_2$  must be chosen so that (at the right end of the truncated cone) we have  $r = b$  (when  $x = L$ ); therefore,  $c_2 = (b - a)/L$ . Our expression, then, becomes

$$r = a + \left( \frac{b-a}{L} \right) x.$$

Substituting this into our previous statement and solving for the field, we find

$$E = \frac{i\rho}{\pi} \left( a + \frac{b-a}{L} x \right)^{-2}.$$

Consequently, the potential difference between the faces of the cone is

$$\begin{aligned} V &= - \int_0^L E \, dx = - \frac{i\rho}{\pi} \int_0^L \left( a + \frac{b-a}{L} x \right)^{-2} dx = \frac{i\rho}{\pi} \frac{L}{b-a} \left( a + \frac{b-a}{L} x \right)^{-1} \Big|_0^L \\ &= \frac{i\rho}{\pi} \frac{L}{b-a} \left( \frac{1}{a} - \frac{1}{b} \right) = \frac{i\rho}{\pi} \frac{L}{b-a} \frac{b-a}{ab} = \frac{i\rho L}{\pi ab}. \end{aligned}$$

The resistance is therefore

$$R = \frac{V}{i} = \frac{\rho L}{\pi ab} = \frac{(731 \, \Omega \cdot \text{m})(1.94 \times 10^{-2} \, \text{m})}{\pi(2.00 \times 10^{-3} \, \text{m})(2.30 \times 10^{-3} \, \text{m})} = 9.81 \times 10^5 \, \Omega$$

Note that if  $b = a$ , then  $R = \rho L / \pi a^2 = \rho L / A$ , where  $A = \pi a^2$  is the cross-sectional area of the cylinder.

34. From Eq. 26-25,  $\rho \propto \bar{\tau}^{-1} \propto v_{\text{eff}}$ . The connection with  $v_{\text{eff}}$  is indicated in part (b) of Sample Problem 26-6, which contains useful insight regarding the problem we are working now. According to Chapter 20,  $v_{\text{eff}} \propto \sqrt{T}$ . Thus, we may conclude that  $\rho \propto \sqrt{T}$ .

35. (a) Electrical energy is converted to heat at a rate given by

$$P = \frac{V^2}{R},$$

where  $V$  is the potential difference across the heater and  $R$  is the resistance of the heater.  
Thus,

$$P = \frac{(120 \text{ V})^2}{14 \text{ } \Omega} = 1.0 \times 10^3 \text{ W} = 1.0 \text{ kW}.$$

(b) The cost is given by  $(1.0 \text{ kW})(5.0 \text{ h})(5.0 \text{ cents/kW} \cdot \text{h}) = \text{US\$}0.25$ .

36. Since  $P = iV$ ,  $q = it = Pt/V = (7.0 \text{ W}) (5.0 \text{ h}) (3600 \text{ s/h})/9.0 \text{ V} = 1.4 \times 10^4 \text{ C}$ .

37. The relation  $P = V^2/R$  implies  $P \propto V^2$ . Consequently, the power dissipated in the second case is

$$P = \left( \frac{1.50 \text{ V}}{3.00 \text{ V}} \right)^2 (0.540 \text{ W}) = 0.135 \text{ W}.$$

38. The resistance is  $R = P/i^2 = (100 \text{ W})/(3.00 \text{ A})^2 = 11.1 \text{ } \Omega$ .

39. (a) The power dissipated, the current in the heater, and the potential difference across the heater are related by  $P = iV$ . Therefore,

$$i = \frac{P}{V} = \frac{1250 \text{ W}}{115 \text{ V}} = 10.9 \text{ A}.$$

(b) Ohm's law states  $V = iR$ , where  $R$  is the resistance of the heater. Thus,

$$R = \frac{V}{i} = \frac{115 \text{ V}}{10.9 \text{ A}} = 10.6 \text{ } \Omega.$$

(c) The thermal energy  $E$  generated by the heater in time  $t = 1.0 \text{ h} = 3600 \text{ s}$  is

$$E = Pt = (1250 \text{ W})(3600 \text{ s}) = 4.50 \times 10^6 \text{ J}.$$



40. (a) From  $P = V^2/R$  we find  $R = V^2/P = (120 \text{ V})^2/500 \text{ W} = 28.8 \, \Omega$ .

(b) Since  $i = P/V$ , the rate of electron transport is

$$\frac{i}{e} = \frac{P}{eV} = \frac{500 \text{ W}}{(1.60 \times 10^{-19} \text{ C})(120 \text{ V})} = 2.60 \times 10^{19} / \text{s}.$$

41. (a) From  $P = V^2/R = AV^2 / \rho L$ , we solve for the length:

$$L = \frac{AV^2}{\rho P} = \frac{(2.60 \times 10^{-6} \text{ m}^2)(75.0 \text{ V})^2}{(5.00 \times 10^{-7} \text{ } \Omega \cdot \text{m})(500 \text{ W})} = 5.85 \text{ m}.$$

(b) Since  $L \propto V^2$  the new length should be

$$L' = L \left( \frac{V'}{V} \right)^2 = (5.85 \text{ m}) \left( \frac{100 \text{ V}}{75.0 \text{ V}} \right)^2 = 10.4 \text{ m}.$$

42. The slopes of the lines yield  $P_1 = 8 \text{ mW}$  and  $P_2 = 4 \text{ mW}$ . Their sum (by energy conservation) must be equal to that supplied by the battery:  $P_{\text{batt}} = ( 8 + 4 ) \text{ mW} = 12 \text{ mW}$ .

43. (a) The monthly cost is  $(100 \text{ W}) (24 \text{ h/day}) (31 \text{ day/month}) (6 \text{ cents/kW} \cdot \text{h}) = 446 \text{ cents} = \text{US\$}4.46$ , assuming a 31-day month.

(b)  $R = V^2/P = (120 \text{ V})^2/100 \text{ W} = 144 \text{ } \Omega$ .

(c)  $i = P/V = 100 \text{ W}/120 \text{ V} = 0.833 \text{ A}$ .

44. Assuming the current is along the wire (not radial) we find the current from Eq. 26-4:

$$i = \int |\vec{J}| dA = \int_0^R kr^2 2\pi r dr = \frac{1}{2} k\pi R^4 = 3.50 \text{ A}$$

where  $k = 2.75 \times 10^{10} \text{ A/m}^4$  and  $R = 0.00300 \text{ m}$ . The rate of thermal energy generation is found from Eq. 26-26:  $P = iV = 210 \text{ W}$ . Assuming a steady rate, the thermal energy generated in 40 s is  $(210 \text{ J/s})(3600 \text{ s}) = 7.56 \times 10^5 \text{ J}$ .

45. (a) Using Table 26-1 and Eq. 26-10 (or Eq. 26-11), we have

$$|\vec{E}| = \rho |\vec{J}| = (1.69 \times 10^{-8} \Omega \cdot \text{m}) \left( \frac{2.00 \text{ A}}{2.00 \times 10^{-6} \text{ m}^2} \right) = 1.69 \times 10^{-2} \text{ V/m}.$$

(b) Using  $L = 4.0 \text{ m}$ , the resistance is found from Eq. 26-16:  $R = \rho L/A = 0.0338 \Omega$ . The rate of thermal energy generation is found from Eq. 26-27:

$$P = i^2 R = (2.00 \text{ A})^2 (0.0338 \Omega) = 0.135 \text{ W}.$$

Assuming a steady rate, the thermal energy generated in 30 minutes is  $(0.135 \text{ J/s})(30 \times 60 \text{ s}) = 2.43 \times 10^2 \text{ J}$ .

46. From  $P = V^2/R$ , we have  $R = (5.0 \text{ V})^2/(200 \text{ W}) = 0.125 \text{ } \Omega$ . To meet the conditions of the problem statement, we must therefore set

$$\int_0^L 5.00x \, dx = 0.125 \text{ } \Omega$$

Thus,

$$\frac{5}{2}L^2 = 0.125 \quad \Rightarrow \quad L = 0.224 \text{ m.}$$

47. (a) We use Eq. 26-16 to compute the resistances in SI units:

$$R_C = \rho_C \frac{L_C}{\pi r_C^2} = (2 \times 10^{-6}) \frac{1}{\pi (0.0005)^2} = 2.5 \, \Omega.$$

The voltage follows from Ohm's law:

$$|V_1 - V_2| = V_C = iR_C = 5.1 \, \text{V}.$$

(b) Similarly,

$$R_D = \rho_D \frac{L_D}{\pi r_D^2} = (1 \times 10^{-6}) \frac{1}{\pi (0.00025)^2} = 5.1 \, \Omega$$

and  $|V_2 - V_3| = V_D = iR_D = 10 \, \text{V}$ .

(c) The power is calculated from Eq. 26-27:  $P_C = i^2 R_C = 10 \, \text{W}$ .

(d) Similarly,  $P_D = i^2 R_D = 20 \, \text{W}$ .



48. (a) Current is the transport of charge; here it is being transported “in bulk” due to the volume rate of flow of the powder. From Chapter 14, we recall that the volume rate of flow is the product of the cross-sectional area (of the stream) and the (average) stream velocity. Thus,  $i = \rho A v$  where  $\rho$  is the charge per unit volume. If the cross-section is that of a circle, then  $i = \rho \pi R^2 v$ .

(b) Recalling that a Coulomb per second is an Ampere, we obtain

$$i = (1.1 \times 10^{-3} \text{ C / m}^3) \pi (0.050 \text{ m})^2 (2.0 \text{ m / s}) = 1.7 \times 10^{-5} \text{ A}.$$

(c) The motion of charge is not in the same direction as the potential difference computed in problem 57 of Chapter 25. It might be useful to think of (by analogy) Eq. 7-48; there, the scalar (dot) product in  $P = \vec{F} \cdot \vec{v}$  makes it clear that  $P = 0$  if  $\vec{F} \perp \vec{v}$ . This suggests that a radial potential difference and an axial flow of charge will not together produce the needed transfer of energy (into the form of a spark).

(d) With the assumption that there is (at least) a voltage equal to that computed in problem 60 of Chapter 24, in the proper direction to enable the transference of energy (into a spark), then we use our result from that problem in Eq. 26-26:

$$P = iV = (1.7 \times 10^{-5} \text{ A})(7.8 \times 10^4 \text{ V}) = 1.3 \text{ W}.$$

(e) Recalling that a Joule per second is a Watt, we obtain  $(1.3 \text{ W})(0.20 \text{ s}) = 0.27 \text{ J}$  for the energy that can be transferred at the exit of the pipe.

(f) This result is greater than the 0.15 J needed for a spark, so we conclude that the spark was likely to have occurred at the exit of the pipe, going into the silo.

49. (a) We are told that  $r_B = \frac{1}{2}r_A$  and  $L_B = 2L_A$ . Thus, using Eq. 26-16,

$$R_B = \rho \frac{L_B}{\pi r_B^2} = \rho \frac{2L_A}{\frac{1}{4}\pi r_A^2} = 8R_A = 64\,\Omega.$$

(b) The current densities are assumed uniform.

$$\frac{J_A}{J_B} = \frac{i/\pi r_A^2}{i/\pi r_B^2} = \frac{i/\pi r_A^2}{4i/\pi r_A^2} = 0.25.$$

50. (a) Circular area depends, of course, on  $r^2$ , so the horizontal axis of the graph in Fig. 26-33(b) is effectively the same as the area (enclosed at variable radius values), except for a factor of  $\pi$ . The fact that the current increases linearly in the graph means that  $i/A = J = \text{constant}$ . Thus, the answer is “yes, the current density is uniform.”

(b) We find  $i/(\pi r^2) = (0.005 \text{ A})/(\pi \times 4 \times 10^{-6} \text{ m}^2) = 398 \approx 4.0 \times 10^2 \text{ A/m}^2$ .

51. Using  $A = \pi r^2$  with  $r = 5 \times 10^{-4}$  m with Eq. 26-5 yields

$$|\vec{J}| = \frac{i}{A} = 2.5 \times 10^6 \text{ A/m}^2.$$

Then, with  $|\vec{E}| = 5.3 \text{ V/m}$ , Eq. 26-10 leads to

$$\rho = \frac{5.3 \text{ V/m}}{2.5 \times 10^6 \text{ A/m}^2} = 2.1 \times 10^{-6} \Omega \cdot \text{m}.$$

52. We find the drift speed from Eq. 26-7:

$$v_d = \frac{|\vec{J}|}{ne} = 1.5 \times 10^{-4} \text{ m/s}.$$

At this (average) rate, the time required to travel  $L = 5.0 \text{ m}$  is

$$t = \frac{L}{v_d} = 3.4 \times 10^4 \text{ s}.$$

53. (a) Referring to Fig. 26-34, the electric field would point down (towards the bottom of the page) in the strip, which means the current density vector would point down, too (by Eq. 26-11). This implies (since electrons are negatively charged) that the conduction-electrons would be “drifting” upward in the strip.

(b) Eq. 24-6 immediately gives 12 eV, or (using  $e = 1.60 \times 10^{-19}$  C)  $1.9 \times 10^{-18}$  J for the work done by the field (which equals, in magnitude, the potential energy change of the electron).

(c) Since the electrons don’t (on average) gain kinetic energy as a result of this work done, it is generally dissipated as heat. The answer is as in part (b): 12 eV or  $1.9 \times 10^{-18}$  J.

54. Since  $100\text{ cm} = 1\text{ m}$ , then  $10^4\text{ cm}^2 = 1\text{ m}^2$ . Thus,

$$R = \frac{\rho L}{A} = \frac{(3.00 \times 10^{-7} \Omega \cdot \text{m})(10.0 \times 10^3 \text{ m})}{56.0 \times 10^{-4} \text{ m}^2} = 0.536 \Omega.$$

55. (a) The charge that strikes the surface in time  $\Delta t$  is given by  $\Delta q = i \Delta t$ , where  $i$  is the current. Since each particle carries charge  $2e$ , the number of particles that strike the surface is

$$N = \frac{\Delta q}{2e} = \frac{i \Delta t}{2e} = \frac{(0.25 \times 10^{-6} \text{ A})(3.0 \text{ s})}{2(1.6 \times 10^{-19} \text{ C})} = 2.3 \times 10^{12}.$$

(b) Now let  $N$  be the number of particles in a length  $L$  of the beam. They will all pass through the beam cross section at one end in time  $t = L/v$ , where  $v$  is the particle speed. The current is the charge that moves through the cross section per unit time. That is,  $i = 2eN/t = 2eNv/L$ . Thus  $N = iL/2ev$ . To find the particle speed, we note the kinetic energy of a particle is

$$K = 20 \text{ MeV} = (20 \times 10^6 \text{ eV})(1.60 \times 10^{-19} \text{ J/eV}) = 3.2 \times 10^{-12} \text{ J}.$$

Since  $K = \frac{1}{2}mv^2$ , then the speed is  $v = \sqrt{2K/m}$ . The mass of an alpha particle is (very nearly) 4 times the mass of a proton, or  $m = 4(1.67 \times 10^{-27} \text{ kg}) = 6.68 \times 10^{-27} \text{ kg}$ , so

$$v = \sqrt{\frac{2(3.2 \times 10^{-12} \text{ J})}{6.68 \times 10^{-27} \text{ kg}}} = 3.1 \times 10^7 \text{ m/s}$$

and

$$N = \frac{iL}{2ev} = \frac{(0.25 \times 10^{-6})(20 \times 10^{-2} \text{ m})}{2(1.60 \times 10^{-19} \text{ C})(3.1 \times 10^7 \text{ m/s})} = 5.0 \times 10^3.$$

(c) We use conservation of energy, where the initial kinetic energy is zero and the final kinetic energy is  $20 \text{ MeV} = 3.2 \times 10^{-12} \text{ J}$ . We note, too, that the initial potential energy is  $U_i = qV = 2eV$ , and the final potential energy is zero. Here  $V$  is the electric potential through which the particles are accelerated. Consequently,

$$K_f = U_i = 2eV \Rightarrow V = \frac{K_f}{2e} = \frac{3.2 \times 10^{-12} \text{ J}}{2(1.60 \times 10^{-19} \text{ C})} = 1.0 \times 10^7 \text{ V}.$$



56. (a) Since  $P = i^2 R = J^2 A^2 R$ , the current density is

$$\begin{aligned} J &= \frac{1}{A} \sqrt{\frac{P}{R}} = \frac{1}{A} \sqrt{\frac{P}{\rho L / A}} = \sqrt{\frac{P}{\rho L A}} \\ &= \sqrt{\frac{1.0 \text{ W}}{\pi (3.5 \times 10^{-5} \Omega \cdot \text{m}) (2.0 \times 10^{-2} \text{ m}) (5.0 \times 10^{-3} \text{ m})^2}} = 1.3 \times 10^5 \text{ A / m}^2. \end{aligned}$$

(b) From  $P = iV = JAV$  we get

$$V = \frac{P}{AJ} = \frac{P}{\pi r^2 J} = \frac{1.0 \text{ W}}{\pi (5.0 \times 10^{-3} \text{ m})^2 (1.3 \times 10^5 \text{ A / m}^2)} = 9.4 \times 10^{-2} \text{ V}.$$

57. Let  $R_H$  be the resistance at the higher temperature ( $800^\circ\text{C}$ ) and let  $R_L$  be the resistance at the lower temperature ( $200^\circ\text{C}$ ). Since the potential difference is the same for the two temperatures, the power dissipated at the lower temperature is  $P_L = V^2/R_L$ , and the power dissipated at the higher temperature is  $P_H = V^2 / R_H$ , so  $P_L = (R_H/R_L)P_H$ . Now  $R_L = R_H + \alpha R_H \Delta T$ , where  $\Delta T$  is the temperature difference  $T_L - T_H = -600^\circ\text{C} = -600\text{ K}$ . Thus,

$$P_L = \frac{R_H}{R_H + \alpha R_H \Delta T} P_H = \frac{P_H}{1 + \alpha \Delta T} = \frac{500\text{ W}}{1 + (4.0 \times 10^{-4} / \text{K})(-600\text{ K})} = 660\text{ W}.$$

58. (a) We use  $P = V^2/R \propto V^2$ , which gives  $\Delta P \propto \Delta V^2 \approx 2V \Delta V$ . The percentage change is roughly

$$\Delta P/P = 2\Delta V/V = 2(110 - 115)/115 = -8.6\%.$$

(b) A drop in  $V$  causes a drop in  $P$ , which in turn lowers the temperature of the resistor in the coil. At a lower temperature  $R$  is also decreased. Since  $P \propto R^{-1}$  a decrease in  $R$  will result in an increase in  $P$ , which partially offsets the decrease in  $P$  due to the drop in  $V$ . Thus, the actual drop in  $P$  will be smaller when the temperature dependency of the resistance is taken into consideration.

59. (a) The current is

$$\begin{aligned} i &= \frac{V}{R} = \frac{V}{\rho L / A} = \frac{\pi V d^2}{4 \rho L} \\ &= \frac{\pi (1.20 \text{ V}) [(0.0400 \text{ in.})(2.54 \times 10^{-2} \text{ m/in.})]^2}{4 (1.69 \times 10^{-8} \Omega \cdot \text{m})(33.0 \text{ m})} = 1.74 \text{ A}. \end{aligned}$$

(b) The magnitude of the current density vector is

$$|\vec{J}| = \frac{i}{A} = \frac{4i}{\pi d^2} = \frac{4(1.74 \text{ A})}{\pi [(0.0400 \text{ in.})(2.54 \times 10^{-2} \text{ m/in.})]^2} = 2.15 \times 10^6 \text{ A/m}^2.$$

(c)  $E = V/L = 1.20 \text{ V}/33.0 \text{ m} = 3.63 \times 10^{-2} \text{ V/m}$ .

(d)  $P = Vi = (1.20 \text{ V})(1.74 \text{ A}) = 2.09 \text{ W}$ .

60. (a) Since

$$\rho = RA/L = \pi R d^2 / 4L = \pi (1.09 \times 10^{-3} \, \Omega) (5.50 \times 10^{-3} \, \text{m})^2 / [4(1.60 \, \text{m})] = 1.62 \times 10^{-8} \, \Omega \cdot \text{m},$$

the material is silver.

(b) The resistance of the round disk is

$$R = \rho \frac{L}{A} = \frac{4\rho L}{\pi d^2} = \frac{4(1.62 \times 10^{-8} \, \Omega \cdot \text{m})(1.00 \times 10^{-3} \, \text{m})}{\pi(2.00 \times 10^{-2} \, \text{m})^2} = 5.16 \times 10^{-8} \, \Omega.$$

61. Eq. 26-26 gives the rate of thermal energy production:

$$P = iV = (10.0 \text{ A})(120 \text{ V}) = 1.20 \text{ kW}.$$

Dividing this into the 180 kJ necessary to cook the three hot-dogs leads to the result  $t = 150 \text{ s}$ .

62. (a) We denote the copper wire with subscript  $c$  and the aluminum wire with subscript  $a$ .

$$R = \rho_a \frac{L}{A} = \frac{(2.75 \times 10^{-8} \Omega \cdot \text{m})(1.3 \text{ m})}{(5.2 \times 10^{-3} \text{ m})^2} = 1.3 \times 10^{-3} \Omega.$$

(b) Let  $R = \rho_c L / (\pi d^2 / 4)$  and solve for the diameter  $d$  of the copper wire:

$$d = \sqrt{\frac{4\rho_c L}{\pi R}} = \sqrt{\frac{4(1.69 \times 10^{-8} \Omega \cdot \text{m})(1.3 \text{ m})}{\pi(1.3 \times 10^{-3} \Omega)}} = 4.6 \times 10^{-3} \text{ m}.$$

63. We use  $P = i^2 R = i^2 \rho L/A$ , or  $L/A = P/i^2 \rho$ .

(a) The new values of  $L$  and  $A$  satisfy

$$\left(\frac{L}{A}\right)_{\text{new}} = \left(\frac{P}{i^2 \rho}\right)_{\text{new}} = \frac{30}{4^2} \left(\frac{P}{i^2 \rho}\right)_{\text{old}} = \frac{30}{16} \left(\frac{L}{A}\right)_{\text{old}}.$$

Consequently,  $(L/A)_{\text{new}} = 1.875(L/A)_{\text{old}}$ , and

$$L_{\text{new}} = \sqrt{1.875} L_{\text{old}} = 1.37 L_{\text{old}} \Rightarrow \frac{L_{\text{new}}}{L_{\text{old}}} = 1.37.$$

(b) Similarly, we note that  $(LA)_{\text{new}} = (LA)_{\text{old}}$ , and

$$A_{\text{new}} = \sqrt{1/1.875} A_{\text{old}} = 0.730 A_{\text{old}} \Rightarrow \frac{A_{\text{new}}}{A_{\text{old}}} = 0.730.$$



64. The horsepower required is

$$P = \frac{iV}{0.80} = \frac{(10\text{ A})(12\text{ V})}{(0.80)(746\text{ W/hp})} = 0.20\text{ hp}.$$

65. We find the current from Eq. 26-26:  $i = P/V = 2.00$  A. Then, from Eq. 26-1 (with constant current), we obtain

$$\Delta q = i\Delta t = 2.88 \times 10^4 \text{ C} \quad .$$

66. We find the resistance from  $A = \pi r^2$  and Eq. 26-16:

$$R = \rho \frac{L}{A} = (1.69 \times 10^{-8}) \frac{45}{1.3 \times 10^{-5}} = 0.061 \, \Omega \quad .$$

Then the rate of thermal energy generation is found from Eq. 26-28:  $P = V^2/R = 2.4 \text{ kW}$ . Assuming a steady rate, the thermal energy generated in 40 s is  $(2.4)(40) = 95 \text{ kJ}$ .

67. We find the rate of energy consumption from Eq. 26-28:

$$P = \frac{V^2}{R} = \frac{90^2}{400} = 20.3 \text{ W} \quad .$$

Assuming a steady rate, the energy consumed is  $(20.3 \text{ J/s})(2.00 \times 3600 \text{ s}) = 1.46 \times 10^5 \text{ J}$ .

68. We use Eq. 26-28:

$$R = \frac{V^2}{P} = \frac{200^2}{3000} = 13.3 \, \Omega \quad .$$

69. The slope of the graph is  $P = 5.0 \times 10^{-4} \text{ W}$ . Using this in the  $P = V^2/R$  relation leads to  $V = 0.10 \text{ Vs}$ .

70. The rate at which heat is being supplied is  $P = iV = (5.2 \text{ A})(12 \text{ V}) = 62.4 \text{ W}$ . Considered on a one-second time-frame, this means 62.4 J of heat are absorbed the liquid each second. Using Eq. 18-16, we find the heat of transformation to be

$$L = \frac{Q}{m} = \frac{62.4 \text{ J}}{21 \times 10^{-6} \text{ kg}} = 3.0 \times 10^6 \text{ J/kg} .$$

71. (a) The current is  $4.2 \times 10^{18} e$  divided by 1 second. Using  $e = 1.60 \times 10^{-19} \text{ C}$  we obtain 0.67 A for the current.

(b) Since the electric field points away from the positive terminal (high potential) and towards the negative terminal (low potential), then the current density vector (by Eq. 26-11) must also point towards the negative terminal.



72. Combining Eq. 26-28 with Eq. 26-16 demonstrates that the power is inversely proportional to the length (when the voltage is held constant, as in this case). Thus, a new length equal to 7/8 of its original value leads to

$$P = \frac{8}{7} (2.0 \text{ kW}) = 2.4 \text{ kW} \quad .$$

73. (a) Since the field is considered to be uniform inside the wire, then its magnitude is, by Eq. 24-42,

$$|\vec{E}| = \frac{|\Delta V|}{L} = \frac{50}{200} = 0.25 \text{ V / m.}$$

Using Eq. 26-11, with  $\rho = 1.7 \times 10^{-8} \Omega \cdot \text{m}$ , we obtain

$$\vec{E} = \rho \vec{J} \Rightarrow \vec{J} = 1.5 \times 10^7 \hat{i}$$

in SI units (A/m<sup>2</sup>).

(b) The electric field points towards lower values of potential (see Eq. 24-40) so  $\vec{E}$  is directed towards point *B* (which we take to be the  $\hat{i}$  direction in our calculation).

74. We use Eq. 26-17:  $\rho - \rho_0 = \rho\alpha(T - T_0)$ , and solve for  $T$ :

$$T = T_0 + \frac{1}{\alpha} \left( \frac{\rho}{\rho_0} - 1 \right) = 20^\circ \text{C} + \frac{1}{4.3 \times 10^{-3} / \text{K}} \left( \frac{58 \Omega}{50 \Omega} - 1 \right) = 57^\circ \text{C}.$$

We are assuming that  $\rho/\rho_0 = R/R_0$ .

75. (a) With  $\rho = 1.69 \times 10^{-8} \Omega \cdot \text{m}$  (from Table 26-1) and  $L = 1000 \text{ m}$ , Eq. 26-16 leads to

$$A = \rho \frac{L}{R} = (1.69 \times 10^{-8}) \frac{1000}{33} = 5.1 \times 10^{-7} \text{ m}^2 .$$

Then,  $A = \pi r^2$  yields  $r = 4.0 \times 10^{-4} \text{ m}$ ; doubling that gives the diameter as  $8.1 \times 10^{-4} \text{ m}$ .

(b) Repeating the calculation in part (a) with  $\rho = 2.75 \times 10^{-8} \Omega \cdot \text{m}$  leads to a diameter of  $1.0 \times 10^{-3} \text{ m}$ .

76. (a) The charge  $q$  that flows past any cross section of the beam in time  $\Delta t$  is given by  $q = i\Delta t$ , and the number of electrons is  $N = q/e = (i/e) \Delta t$ . This is the number of electrons that are accelerated. Thus

$$N = \frac{(0.50 \text{ A})(0.10 \times 10^{-6} \text{ s})}{1.60 \times 10^{-19} \text{ C}} = 3.1 \times 10^{11}.$$

(b) Over a long time  $t$  the total charge is  $Q = nqt$ , where  $n$  is the number of pulses per unit time and  $q$  is the charge in one pulse. The average current is given by  $i_{\text{avg}} = Q/t = nq$ . Now  $q = i\Delta t = (0.50 \text{ A})(0.10 \times 10^{-6} \text{ s}) = 5.0 \times 10^{-8} \text{ C}$ , so

$$i_{\text{avg}} = (500 / \text{s})(5.0 \times 10^{-8} \text{ C}) = 2.5 \times 10^{-5} \text{ A}.$$

(c) The accelerating potential difference is  $V = K/e$ , where  $K$  is the final kinetic energy of an electron. Since  $K = 50 \text{ MeV}$ , the accelerating potential is  $V = 50 \text{ kV} = 5.0 \times 10^7 \text{ V}$ . The average power is

$$P_{\text{avg}} = i_{\text{avg}} V = (2.5 \times 10^{-5} \text{ A})(5.0 \times 10^7 \text{ V}) = 1.3 \times 10^3 \text{ W}.$$

(d) During a pulse the power output is

$$P = iV = (0.50 \text{ A})(5.0 \times 10^7 \text{ V}) = 2.5 \times 10^7 \text{ W}.$$

This is the peak power.

77. The power dissipated is given by the product of the current and the potential difference:  $P = iV = (7.0 \times 10^{-3} \text{ A})(80 \times 10^3 \text{ V}) = 560 \text{ W}$ .

78. (a) Let  $\Delta T$  be the change in temperature and  $\kappa$  be the coefficient of linear expansion for copper. Then  $\Delta L = \kappa L \Delta T$  and

$$\frac{\Delta L}{L} = \kappa \Delta T = (1.7 \times 10^{-5} / \text{K})(1.0^\circ \text{C}) = 1.7 \times 10^{-5}.$$

This is equivalent to 0.0017%. Since a change in Celsius is equivalent to a change on the Kelvin temperature scale, the value of  $\kappa$  used in this calculation is not inconsistent with the other units involved. Incorporating a factor of 2 for the two-dimensional nature of  $A$ , the fractional change in area is

$$\frac{\Delta A}{A} = 2\kappa \Delta T = 2(1.7 \times 10^{-5} / \text{K})(1.0^\circ \text{C}) = 3.4 \times 10^{-5}$$

which is 0.0034%. For small changes in the resistivity  $\rho$ , length  $L$ , and area  $A$  of a wire, the change in the resistance is given by

$$\Delta R = \frac{\partial R}{\partial \rho} \Delta \rho + \frac{\partial R}{\partial L} \Delta L + \frac{\partial R}{\partial A} \Delta A.$$

Since  $R = \rho L/A$ ,  $\partial R/\partial \rho = L/A = R/\rho$ ,  $\partial R/\partial L = \rho/A = R/L$ , and  $\partial R/\partial A = -\rho L/A^2 = -R/A$ . Furthermore,  $\Delta \rho/\rho = \alpha \Delta T$ , where  $\alpha$  is the temperature coefficient of resistivity for copper ( $4.3 \times 10^{-3}/\text{K} = 4.3 \times 10^{-3}/\text{C}^\circ$ , according to Table 26-1). Thus,

$$\begin{aligned} \frac{\Delta R}{R} &= \frac{\Delta \rho}{\rho} + \frac{\Delta L}{L} - \frac{\Delta A}{A} = (\alpha + \kappa - 2\kappa) \Delta T = (\alpha - \kappa) \Delta T \\ &= (4.3 \times 10^{-3} / \text{C}^\circ - 1.7 \times 10^{-5} / \text{C}^\circ)(1.0 \text{C}^\circ) = 4.3 \times 10^{-3}. \end{aligned}$$

This is 0.43%, which we note (for the purposes of the next part) is primarily determined by the  $\Delta \rho/\rho$  term in the above calculation.

(b) As shown in part (a), the percentage change in  $L$  is 0.0017%.

(c) As shown in part (a), the percentage change in  $A$  is 0.0034%.

(d) The fractional change in resistivity is much larger than the fractional change in length and area. Changes in length and area affect the resistance much less than changes in resistivity.

79. (a) In Eq. 26-17, we let  $\rho = 2\rho_0$  where  $\rho_0$  is the resistivity at  $T_0 = 20^\circ\text{C}$ :

$$\rho - \rho_0 = 2\rho_0 - \rho_0 = \rho_0\alpha(T - T_0),$$

and solve for the temperature  $T$ :

$$T = T_0 + \frac{1}{\alpha} = 20^\circ\text{C} + \frac{1}{4.3 \times 10^{-3} / \text{K}} \approx 250^\circ\text{C}.$$

(b) Since a change in Celsius is equivalent to a change on the Kelvin temperature scale, the value of  $\alpha$  used in this calculation is not inconsistent with the other units involved. It is worth noting that this agrees well with Fig. 26-10.



80. Since values from the referred-to graph can only be crudely estimated, we do not present a graph here, but rather indicate a few values. Since  $R = V/i$  then we see  $R = \infty$  when  $i = 0$  (which the graph seems to show throughout the range  $-\infty < V < 2 \text{ V}$ ) and  $V \neq 0$ . For voltages values larger than  $2 \text{ V}$ , the resistance changes rapidly according to the ratio  $V/i$ . For instance,  $R \approx 3.1/0.002 = 1550 \text{ } \Omega$  when  $V = 3.1 \text{ V}$ , and  $R \approx 3.8/0.006 = 633 \text{ } \Omega$  when  $V = 3.8 \text{ V}$ .

$$81. (a) V = iR = i\rho \frac{L}{A} = \frac{(12 \text{ A})(1.69 \times 10^{-8} \Omega \cdot \text{m})(4.0 \times 10^{-2} \text{ m})}{\pi(5.2 \times 10^{-3} \text{ m} / 2)^2} = 3.8 \times 10^{-4} \text{ V}.$$

(b) Since it moves in the direction of the electron drift which is against the direction of the current, its tail is negative compared to its head.

(c) The time of travel relates to the drift speed:

$$\begin{aligned} t &= \frac{L}{v_d} = \frac{lAne}{i} = \frac{\pi L d^2 n e}{4i} \\ &= \frac{\pi(1.0 \times 10^{-2} \text{ m})(5.2 \times 10^{-3} \text{ m})^2 (8.47 \times 10^{28} / \text{m}^3)(1.60 \times 10^{-19} \text{ C})}{4(12 \text{ A})} \\ &= 238 \text{ s} = 3 \text{ min } 58 \text{ s}. \end{aligned}$$

82. Using Eq. 7-48 and Eq. 26-27, the rate of change of mechanical energy of the piston-Earth system,  $mgv$ , must be equal to the rate at which heat is generated from the coil:  $mgv = i^2 R$ . Thus

$$v = \frac{i^2 R}{mg} = \frac{(0.240 \text{ A})^2 (550 \Omega)}{(12 \text{ kg})(9.8 \text{ m/s}^2)} = 0.27 \text{ m/s}.$$

83. (a)  $i = (n_h + n_e)e = (2.25 \times 10^{15}/\text{s} + 3.50 \times 10^{15}/\text{s}) (1.60 \times 10^{-19} \text{ C}) = 9.20 \times 10^{-4} \text{ A}.$

(b) The magnitude of the current density vector is

$$|\vec{J}| = \frac{i}{A} = \frac{9.20 \times 10^{-4} \text{ A}}{\pi(0.165 \times 10^{-3} \text{ m})^2} = 1.08 \times 10^4 \text{ A/m}^2.$$